



Swansea University
Prifysgol Abertawe



Cronfa - Swansea University Open Access Repository

This is an author produced version of a paper published in:

Desalination

Cronfa URL for this paper:

<http://cronfa.swan.ac.uk/Record/cronfa38388>

Paper:

Loganathan, K., Saththasivam, J. & Sarp, S. (2018). Removal of microalgae from seawater using chitosan-alum/ferric chloride dual coagulations. *Desalination*, 433, 25-32.

<http://dx.doi.org/10.1016/j.desal.2018.01.012>

This item is brought to you by Swansea University. Any person downloading material is agreeing to abide by the terms of the repository licence. Copies of full text items may be used or reproduced in any format or medium, without prior permission for personal research or study, educational or non-commercial purposes only. The copyright for any work remains with the original author unless otherwise specified. The full-text must not be sold in any format or medium without the formal permission of the copyright holder.

Permission for multiple reproductions should be obtained from the original author.

Authors are personally responsible for adhering to copyright and publisher restrictions when uploading content to the repository.

<http://www.swansea.ac.uk/library/researchsupport/ris-support/>

1 **Removal of microalgae from seawater using Chitosan-alum/ferric chloride dual coagulations**

2 Kavithaa Loganathan¹, Jayaprakash Saththasivam¹, Sarp Sarper*²

3 ¹ P.O. Box: 34110, Qatar Environment and Energy Research Institute (QEERI), Hamad Bin Khalifa University
4 (HBKU), Qatar Foundation, Doha, Qatar

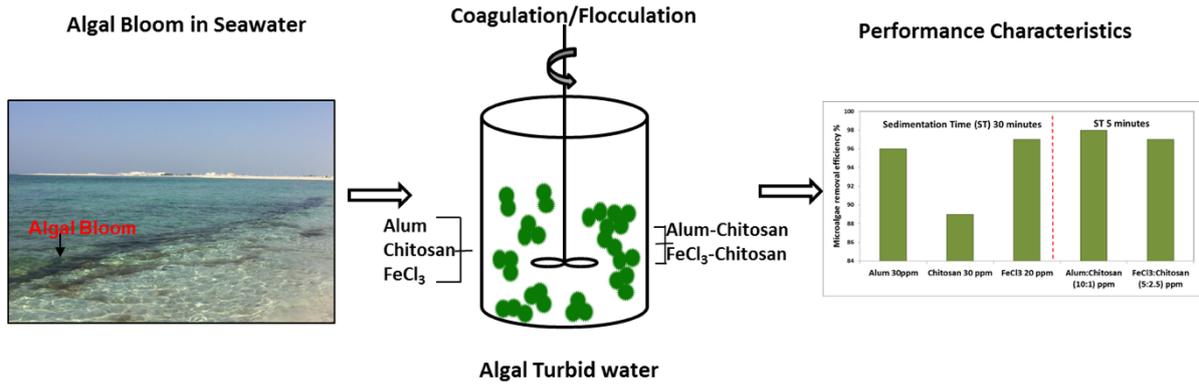
5 ² Centre for Water Advanced Technologies and Environmental Research (CWATER), College of Engineering,
6 Swansea University, Fabian Way, Swansea SA1 8EN, UK

7 * Corresponding author: email: sarper.sarp@swansea.ac.uk

8

9 **Graphical Abstract:**

10



11

12

1 **Highlights:**

- 2 • Coagulation-flocculation-sedimentation (C-F-S) experiments using FeCl₃ coagulant gave
3 better process performance when compared to alum and chitosan based individual
4 coagulations
- 5 • Dual coagulation using alum as coagulant and chitosan as flocculent aid improved
6 microalgae removal efficiency at a reduced process time, thus making C-F-S process as
7 attractive as Coagulation-flocculation-dissolved air flotation (C-F-D) process
- 8 • Residual alum concentration in dual coagulation process was significantly reduced when
9 compared to alum based individual coagulation

10

Removal of microalgae from seawater using Chitosan-alum/ferric chloride dual coagulations

Kavithaa Loganathan¹, Jayaprakash Saththasivam¹, Sarp Sarper*²

¹ P.O. Box: 34110, Qatar Environment and Energy Research Institute (QEERI), Hamad Bin Khalifa University (HBKU), Qatar Foundation, Doha, Qatar

² Centre for Water Advanced Technologies and Environmental Research (CWATER), College of Engineering, Swansea University, Fabian Way, Swansea SA1 8EN, UK

* Corresponding author: email: sarper.sarp@swansea.ac.uk

Abstract

During algal bloom, it's a challenge to provide good quality feed water, and ensure sustainable RO plant operations without an adequate pre-treatment of seawater. In this paper, the effectiveness of the coagulation process with the individual and dual coagulants, using alum, FeCl₃ and chitosan, were explored aiming to remove microalgae from seawater. The coagulation-flocculation-sedimentation (C-F-S) experiments were conducted by optimizing multiple process strategies to reduce the amounts of coagulants and also to shorten the sedimentation process time. The coagulation-flocculation-dissolved air flotation (C-F-D) experiments were performed to generate the process data in order to evaluate the dual coagulation process performance of the C-F-S system. C-F-S experiments using FeCl₃ coagulant gave better process performance (20 ppm FeCl₃ dose, 8.2 pH, 30 min sedimentation time and 98% microalgae removal efficiency) when compared to alum and chitosan based individual coagulations. The process time of the coagulation process was significantly reduced by the addition of chitosan as a flocculent aid. For dual coagulation using alum (10 ppm) as coagulant and chitosan (1ppm) as flocculent aid improved microalgae removal efficiency to 98% at a reduced process time of 5 minutes, making C-F-S process as attractive as C-F-D process.

Keywords: Harmful algal bloom (HAB); sustainable seawater feed; microalgae removal; dual coagulation; bioflocculant; coagulation-flocculation-sedimentation process

1 Introduction

More than half of the world's population lives in water stress areas, and the numbers are expected to increase to two-thirds by 2025. In many parts of the world, shortage of fresh water is a looming crisis due to climate change and the increase of the global population [1]. Seawater desalination is one of the feasible solutions in addressing the water crisis [2-6]. Reverse osmosis (RO) is a widely used technology for desalinating seawater [7]. However, sustainable operations of seawater reverse osmosis (SWRO) plants depend on the quality of the feed water. Seasonal microalgae blooms are one of the operational challenges faced by SWRO operators, where blooms can hamper the performance of the plant and potable water quality [8-13]. Apart from inducing particulate fouling on the membrane which results in sporadic plant disruptions [14-17], microalgae has a tendency to release potent toxins into the water when its cells are ruptured due to trans-membrane pressure. These toxins pose severe health problems in humans [18-21], resulting in dermatologic, gastrointestinal, respiratory, and neurologic disorders. The focus of this work is to improve performance of pre-treatment processes to produce microalgae free feed water for SWRO plants.

There are several treatment options available to remove microalgae from feed water, namely: (i) disinfection (ii) filtration and (iii) physico-chemical removal process. Although chlorination is effective in disinfecting microalgae, the presence of residual chlorine can significantly decrease the lifespan of membranes. Similar to chlorination, other disinfection methods, such as UV

1 and ozone, can result in cell-lysis, which releases toxins into the feed water [22]. Sand
2 filtration/flotation processes are ineffective in removing microalgae, unless preceded by chemical
3 coagulation-flocculation. The retention efficiency of a sand filter obtained for 145,000 cells/ml algae
4 was reported as 80% during the first few hours of filtration and dropped to 48% after 7 hours [23].
5 For the coagulation process, alum and ferric chloride are among the common coagulants used by the
6 water treatment industry. Ferric salts are preferred in sea water desalination, due to the low
7 solubility of the resulting ferric hydroxide in seawater, over a wide range of pH. On the other hand,
8 the use of alum as a cationic coagulant in seawater is not favoured due to the high solubility of
9 aluminium hydroxide in seawater, which leads to the precipitative scaling of RO membranes [12].
10 Natural coagulants have also been used in water treatment processes [24, 25]. Chitosan, a cationic
11 polymer prepared from crab/shrimp shells, is the second most abundant biopolymer in the world
12 after cellulose [26]. Chitosan is positively charged, due to the protonization of amino groups in a
13 solution which makes it attractive for a variety of binding applications.

14 Following coagulation-flocculation, the dissolved air flotation process (C-F-D) is commonly used in
15 the upstream of MF/UF systems to minimize the solid loadings [27-30]. Dissolved air flotation (DAF)
16 is a relatively quick process which is suitable for the removal of low-density algal particles. However,
17 DAF is an energy intensive process (0.05-0.075 kWh/m³ of treated water)[31], as the generation of
18 air microbubbles requires compressed air requiring as high as 7 bars. Another option to remove
19 microalgae is by the coagulation-flocculation-sedimentation (C-F-S) process. However, it is less
20 preferred, as a long settling time is required to achieve a comparable removal rate with DAF.
21 Sedimentation time of the C-F-S process using some common coagulants for microalgae removal
22 was reported as more than 2 hours [32]. Optimization of the coagulation strategies can achieve the
23 best microalgae removal rate in the shortest time possible. The sedimentation time of microalgae
24 can be shortened by improving the size and density of the flocs. The purpose of this article is to
25 explore the C-F-S process, and flocculation properties of the dual coagulants, alum-chitosan, and
26 FeCl₃-chitosan for microalgae removal in seawater. The dual coagulation strategy was followed to
27 minimize the coagulant dosage, in order to optimize the density of flocs, and to minimize the
28 sedimentation time.

29 **2 Materials and Methods:**

30 In Qatar, the algal bloom season starts in the month of October (Figure 1B) and ends approximately
31 around the month of April, as shown in Figure 1A. Seawater samples analysed during these months
32 revealed that the microalgae counts were around six times higher at the start of bloom season,
33 when compared to the April data (Table 1). Phytoplankton counts were calculated by measuring the
34 chlorophyll intensity of each cell, using a BD Accuri C6 flow cytometer (Ann Arbor, Michigan, USA).
35 The dual threshold triggers on FL3 (Excitation: 488 nm; Emission: 670 nm) and FL4 (Ex: 640 nm; Em:
36 675 ±12.5 nm) were set just above background noise. A 50 µL sample was injected at the medium
37 fluidic settings (35 µL/min; core size 16 µm) in order to obtain the absolute cell counts. Particle size
38 measurements were taken by using a Jorin VIPA B HiFlo analyser (Leicestershire, UK), which
39 indicated that the microalgae size was between 2-5 µm. In addition to microalgae, macroalgal
40 deposits were found on the shore (Figure 1 Captions 'C1 and C2'). These blooms can cause
41 ecological, and societal impacts, including the disruption of the intake of water for
42 cooling/desalination[12].



Table 1 Raw sea water analysis		
Date	Apr-16	Oct-16
Algal Cell Counts		
Cells per μL	18	106
pH	8.15	8.24
Turbidity NTU	0.98	3.1
Alkalinity ppm	128.8	126.8
Total Hardness		
ppm	10,150	10,209
Calcium Hardness		
ppm	1,800	1,839
TDS ppm	49,228	49,115



1

2 **Figure 1:** Sea water in April 2016 (clear season) and Oct 2016 (start of bloom season). Pictures C1 &
 3 C2 shows macro algae deposits during bloom season. The pictures were taken near the desalination
 4 plant in Qatar, for this project.

5 The seawater samples were collected from the west coast of Qatar, in bulk, to prepare the
 6 microalgae culture solution. NKP salts were added, as per the literature method [33], on a weekly
 7 basis to the sea water in order to enhance algae growth. The purpose of using a sea water culture is
 8 to reflect heavy bloom conditions, with microalgae cell counts $\sim 1.5 \times 10^3$ per μL , and to maintain the
 9 consistency of the algae model solution during the testing period.

10 Jar tests were carried out by using a programmable apparatus (Phipps & Bird, USA) at room
 11 temperature. The tester was programmed for rapid mixing at 100 RPM for one minute; slow mixing
 12 at 30 RPM for 15 minutes; followed by sedimentation for 30 minutes [34]. Residual aluminium
 13 concentration was determined using Agilent inductively coupled plasma-mass spectrometer (ICP-MS
 14 7500c), equipped with automatic sampler introduction and with concentric and microflow
 15 nebulization. For dual coagulation using alum, two sets of experiments were conducted as shown in
 16 Figure 2. Firstly, an alum and chitosan mixture was used as a primary coagulant, which was added
 17 during the rapid mixing and the coagulation stage. The second set of experiments were conducted
 18 using alum as the primary coagulant and chitosan as the secondary coagulant which acted as a
 19 flocculant aid. The primary coagulant was added during the rapid mixing stage, and the secondary
 20 was added during the slow mixing stage.

1 About 100 mL of samples were taken after the sedimentation stage for analyses. Similar experiments
 2 were conducted using FeCl_3 as the primary coagulant, and chitosan, as a flocculent aid.

3 DAF jar tests were performed using the batch jar tester Platypus DAF system, with a 2L capacity DAF
 4 saturator. For DAF particle separation experiments, coagulation and flocculation processes were
 5 followed by a 10 minute period of flotation, using a 15-30% recycling ratio at a saturation pressure of
 6 675 kPa [28]. The operational conditions of coagulation/flocculation are similar to the
 7 sedimentation studies. The DAF-treated samples were collected via sampling ports for
 8 characterization studies (microbial counts, turbidity). The C-F-D process was performed using alum
 9 and FeCl_3 as coagulants, mainly to generate the process data in order to evaluate the dual
 10 coagulation process performance of the C-F-S system.

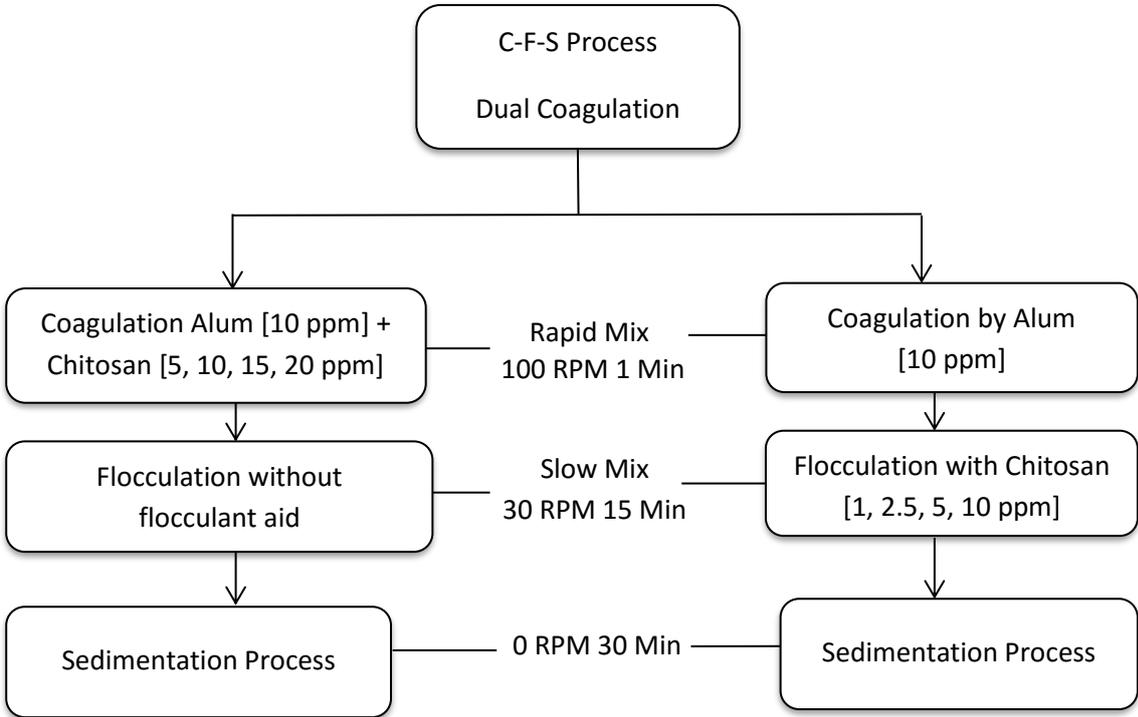


Figure 2: Flowchart indicating the stages of dual C-F-S process

3 Results and Discussion:

3.1 Coagulation studies with Alum, Chitosan and FeCl_3

The jar test experiments were conducted with alum, chitosan and ferric chloride coagulants to determine the optimal coagulant dose, based on settled water turbidity (Figure 3A). The clarified water turbidity, decreased with coagulant additions to the levels (0.7, 2.7 and 0.5 NTU for alum, chitosan and FeCl_3 respectively), after which turbidity increased. The optimum dose of alum, chitosan, and FeCl_3 for maximum turbidity removal was found to be 30, 30 and 20 mg/L respectively. The corresponding micro algae removal efficiency of alum, chitosan and FeCl_3 were found to be 96.3, 87.3 and 98.6 % respectively (Table 2).

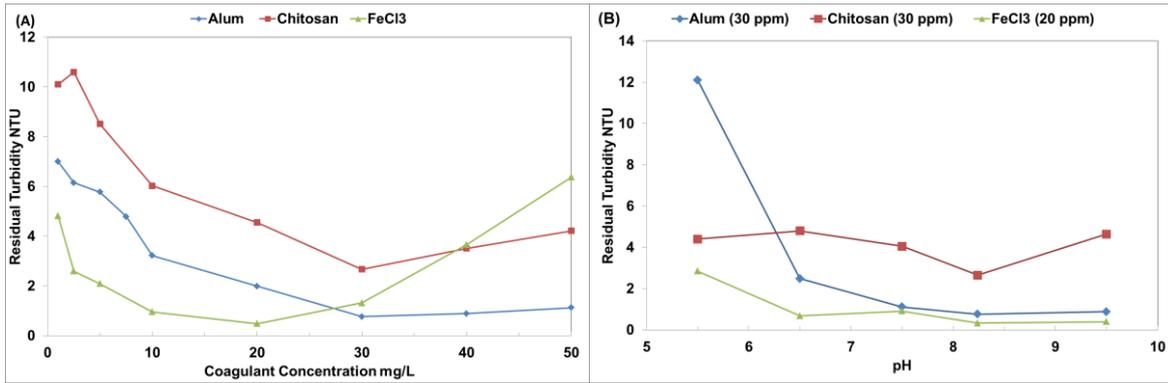


Figure 3. Residual turbidity versus coagulant dose for alum, chitosan and ferric chloride (A); pH (B)

An overdose of alum (50 ppm) caused charge reversal which led to decrease in microalgae removal efficiency (Figure 4 A) and increase in turbidity values. An overdose of chitosan led to an increase in turbidity values, while the microalgae removal efficiency remained constant 87% (Figure 4B). Furthermore, the higher ferric chloride dose increased the turbidity values; while higher microalgae removal efficiency was observed (Figure 4E). Results show the importance of both microalgae cells counts, and turbidity measurements, to determine the extent of the coagulation process. Compared to alum and chitosan coagulants, FeCl₃ required the least amount of dosage to achieve the greatest amount of turbidity, and microalgae removal. With the optimized coagulants dose levels, the pH for maximum turbidity removal occurred at raw water with a pH of 8.2, as shown in Figure 3B. Therefore, the experiments were conducted with microalgae cultured seawater samples without pH adjustments. Clarified water was filtered using 0.45 micron filter, and characterized for residual aluminium concentration using ICP-MS. At 22°C and pH 8.2, and the residual aluminium concentration was found to be 697 µg/L. For Chitosan coagulation DOC ranges between 0.1 and 0.4 ppm.

Table2: Results of seawater (individual, dual) coagulation with coagulants alum, chitosan and FeCl₃

Coagulant Dose ppm	pH	Turbidity NTU	Microalgae Cell Counts Per µL	% Removal	Sedimentation Time Minutes	
Alum Coagulation						Residual Al ppb
Raw Water	8.2	37	1579			-
1	8.2	7	1233	21.9	30	490.1
2.5	8.2	6.15	1150	27.2	30	502.6
5	8.2	5.78	1035	34.5	30	540.8
7.5	8.2	4.79	874	44.6	30	554.2
10	8.2	3.22	270	82.9	30	590.8
20	8.2	1.99	108	93.2	30	590.7
30	8.2	0.77	58	96.3	30	697.2
40	8.2	0.89	215	86.4	30	701.3
50	8.2	1.13	818	48.2	30	750.5
30	5.5	12.1	1623	-	30	790.6
30	6.5	2.49	538	65.9	30	750.8

30	7.5	1.12	255	83.9	30	742.5
30	8.2	0.77	58	96.3	30	697.2
30	9.5	0.89	82	94.8	30	790.5
Chitosan Coagulation						DOC ppm
Raw Water	8.2	21.1	1827			
1	8.2	10.1	1470	19.5	30	0.1
2.5	8.2	10.6	1370	25.0	30	0.2
5	8.2	8.51	1249	31.6	30	0.2
10	8.2	6.03	588	67.8	30	0.4
20	8.2	4.55	377	79.4	30	0.2
30	8.2	2.67	274	89.6	30	0.3
40	8.2	3.51	267	89.9	30	0.2
50	8.2	4.22	273	89.6	30	0.4
20	5.5	4.41	240	90.9	30	-
20	6.5	4.8	287	89.1	30	-
20	7.5	4.06	239	90.9	30	-
20	8.2	2.66	325	87.7	30	-
20	9.5	4.65	817	69.0	30	-
Alum (A) : Chitosan (Ch; Coagulation aid)						Residual Al ppb
Raw Water	8.2	15	1639			
10 A:00 Ch	8.2	3.22	270	83.5	30	-
10 A:05 Ch	8.2	1.5	154	90.5	30	150
10 A:10 Ch	8.2	2.11	590	64.0	30	-
10 A:15 Ch	8.2	4	900	45.1	30	-
10 A:20 Ch	8.2	6.8	1462	10.8	30	-
Alum (A) : Chitosan (Ch; Flocculation aid)						
Raw Water	8.2	22.2	1636			-
10 A:01 Ch	8.2	1.11	39	97.6	5	67
10 A:2.5 Ch	8.2	1.5	48	97.1	5	-
10 A:05 Ch	8.2	1.21	73	95.5	5	-
10 A:10 Ch	8.2	1.22	74	95.5	5	-
FeCl₃ Coagulation						Residual Fe ppm
Raw Water	8.2	15.5	1430			
1	8.2	4.81	672	53.0	30	<0.1
2.5	8.2	2.6	357	75.0	30	<0.1
5	8.2	2.09	215	85.0	30	0.11
10	8.2	0.96	78	94.5	30	0.16
20	8.2	0.49	20	98.6	30	<0.1
30	8.2	1.32	16	98.9	30	0.15
40	8.2	3.66	13	99.1	30	0.82
50	8.2	6.37	8	99.4	30	2.90
20	5.5	2.85	37	97.4	30	-

20	6.5	0.68	34	97.6	30	-
20	7.5	0.91	52	96.4	30	<0.1
20	8.2	0.33	20	98.6	30	<0.1
20	9.5	0.4	25	98.3	30	-
FeCl₃ (I):Chitosan (Ch; flocculation aid)						
Raw Water	8.2	15	1744			-
5(I):0.5(Ch)	8.2	2.28	106	93.9	5	-
5(I):1.0(Ch)	8.2	2.56	67	96.1	5	-
5(I):2.5(Ch)	8.2	1.25	48	97.2	5	<0.1
5(I):5.0(Ch)	8.2	2.27	84	95.1	5	-
5(I):10(Ch)	8.2	2.05	128	92.6	5	-

1

2

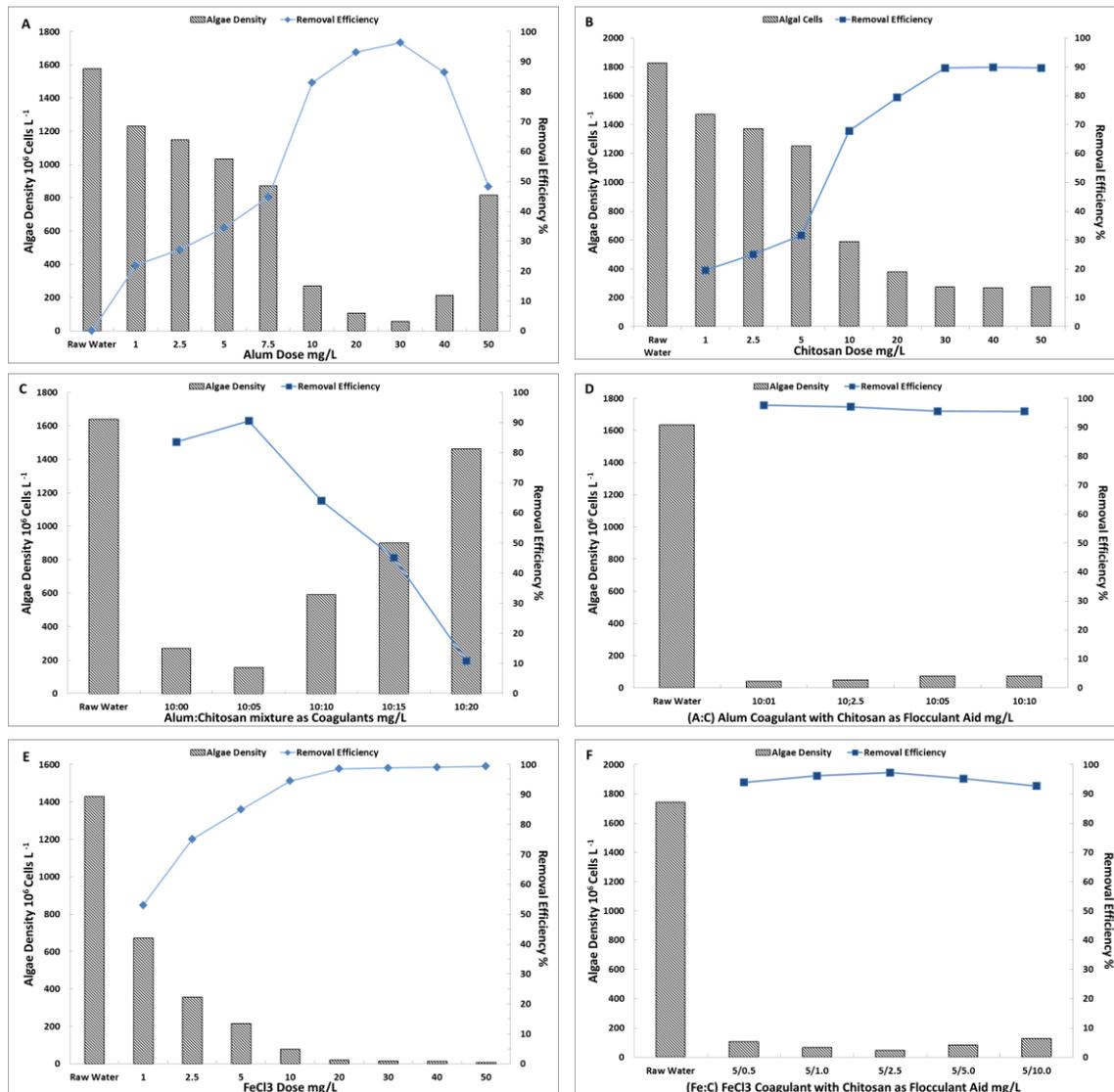


Figure 4: Dosage effects on coagulation performance of A: alum B. chitosan C. alum:chitosan mixture D. alum primary coagulant with chitosan as flocculent aid E. FeCl_3 F. FeCl_3 primary coagulant with chitosan as flocculent aid

1

2 **3.2 Performance of C-F-D Process:**

3 In this study, the DAF performance as a particle separation method for microalgae removal was
 4 investigated for alum and FeCl_3 coagulation processes. In the DAF process, air was added to a
 5 suspension of flocculated water to induce buoyancy, which drove the floc-bubble aggregates to the
 6 top of the DAF reactor towards the float layer. At the end of flotation process, clarified seawater
 7 samples were collected, and characterized using flow cytometer and turbidity measurements to
 8 obtain microalgae removal efficiency. It has been seen that the high ionic strength of seawater
 9 affects the performance of the DAF process, and therefore the design corrections were followed to
 10 maximize the DAF performance, as recommended by Edzwald [1]. The seawater saturation pressure
 11 was maintained at 675 kPa, and the recycle rate was varied from 15% to 30% to optimize the DAF
 12 performance, targeting microalgae removal. For alum (10 ppm) coagulation, the DAF particle
 13 separation process resulted in around 94% of microalgae removal in less than two minutes of

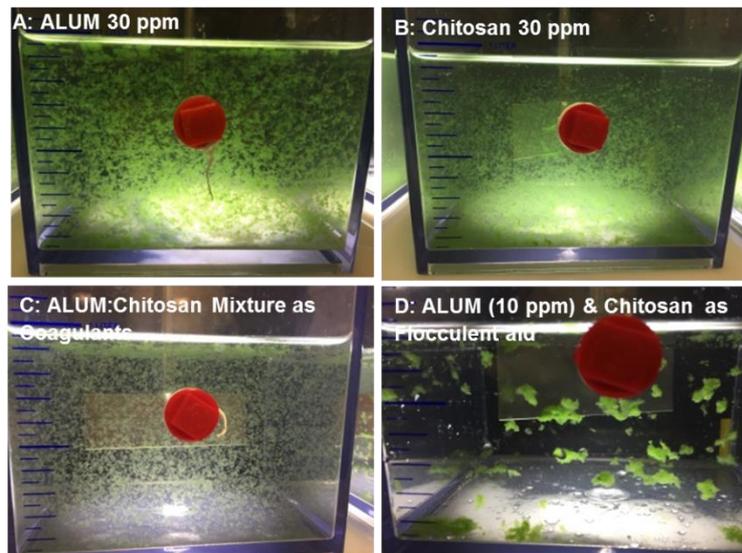
1 flotation time (Table 3). Only 84% microalgae removal was achieved with 10 ppm alum
 2 concentration, using a sedimentation process with the settling time of around 30 minutes (Figure
 3 4a). Similarly, a more efficient (ca.94%) microalgae removal was achieved for FeCl₃ [5 ppm]
 4 coagulation using the process, with less than two minutes flotation time as compared to the 30
 5 minutes settling time required for C-F-S process.

6 **Table 3 Performance of C-F-D process in microalgae removal from seawater**

Coagulant	Coagulant Dose mg/L	Flotation Recycling Ratio %	Saturation Pressure kPa	Microalgae Removal Efficiency %
Alum	10	15	675	93.7
Alum	10	30	675	94.1
FeCl ₃	5	15	675	94.7
FeCl ₃	5	30	675	94.2

7
 8 *3.3 Reduction of Coagulant Dose and sedimentation time of C-F-S process through dual coagulation*
 9 *strategy*

10 Dual coagulation experiments were conducted using alum and FeCl₃ as primary coagulants and
 11 Chitosan mainly as a coagulant/flocculant aid. Investigations were aimed to check the possibilities of
 12 reducing primary coagulant dosage and to minimize the sedimentation time. When the coagulation
 13 experiments are compared with alum at 7.5 ppm and 10 ppm dosage levels, a sharp increase (from
 14 44% to 82%) in microalgae removal efficiency was observed (Figure 4A, Table 2). In all dual
 15 coagulation experiments involving alum, the dosage was fixed at 10 ppm. For the first set of
 16 experiments (case1) alum 10 ppm was mixed with a chitosan dosage from 1 to 10 mg/L (Figure 4C)
 17 and the mixture was added during the rapid mixing stage of the coagulation process. A maximum
 18 microalgae removal of 90.5% was achieved for alum 10 ppm: chitosan 5 ppm mixture. A further
 19 increase in chitosan concentration resulted in a sharp decrease in microalgae removal efficiency. A
 20 sedimentation time of 30 minutes was required for case 1 experiments. The re-stabilisation
 21 behaviour was characterized by the appearance of smaller flocs as shown in Figure 5C. Clarified
 22 water was filtered using 0.45 micron filter, and the residual aluminium concentration was found to
 23 be 150 µg/L.



1 Figure 5: Pictures of well-grown flocs taken towards the end of flocculation process. Floc
 2 size for A(Alum 30 ppm)- 2.0 mm to 5.1 mm; B (chitosan 30 ppm)- < 3.0 mm; C
 3 (Alum:Chitosan mixture as coagulants)- 2.7 mm to 4.4 mm; D (Alum 10ppm & Chitosan as
 4 flocculant aid)- 3.8 mm to 12.7 mm

5 For the second set of the dual coagulation experiments (case 2), an alum dose of 10 ppm was added
 6 during the rapid mixing stage, and a chitosan dose was added during the slow mixing/flocculation
 7 stage (Figure 4D, Table 2). The microalgae removal efficiency was over 98%, as shown in Figure 4D.
 8 The optimum removal efficiency was observed for alum:chitosan (10 ppm:1 ppm), which then
 9 plateaued when overdosed with chitosan, with a sedimentation settling time of five minutes.
 10 Furthermore, larger flocs were observed, as shown in Figure 5 D. Clarified water was filtered using
 11 0.45 micron filter, and the residual aluminium concentration was found to be 67 $\mu\text{g/L}$. The dual
 12 coagulation experiments resulted 10 times lower residual aluminium concentration than observed
 13 for alum coagulation.

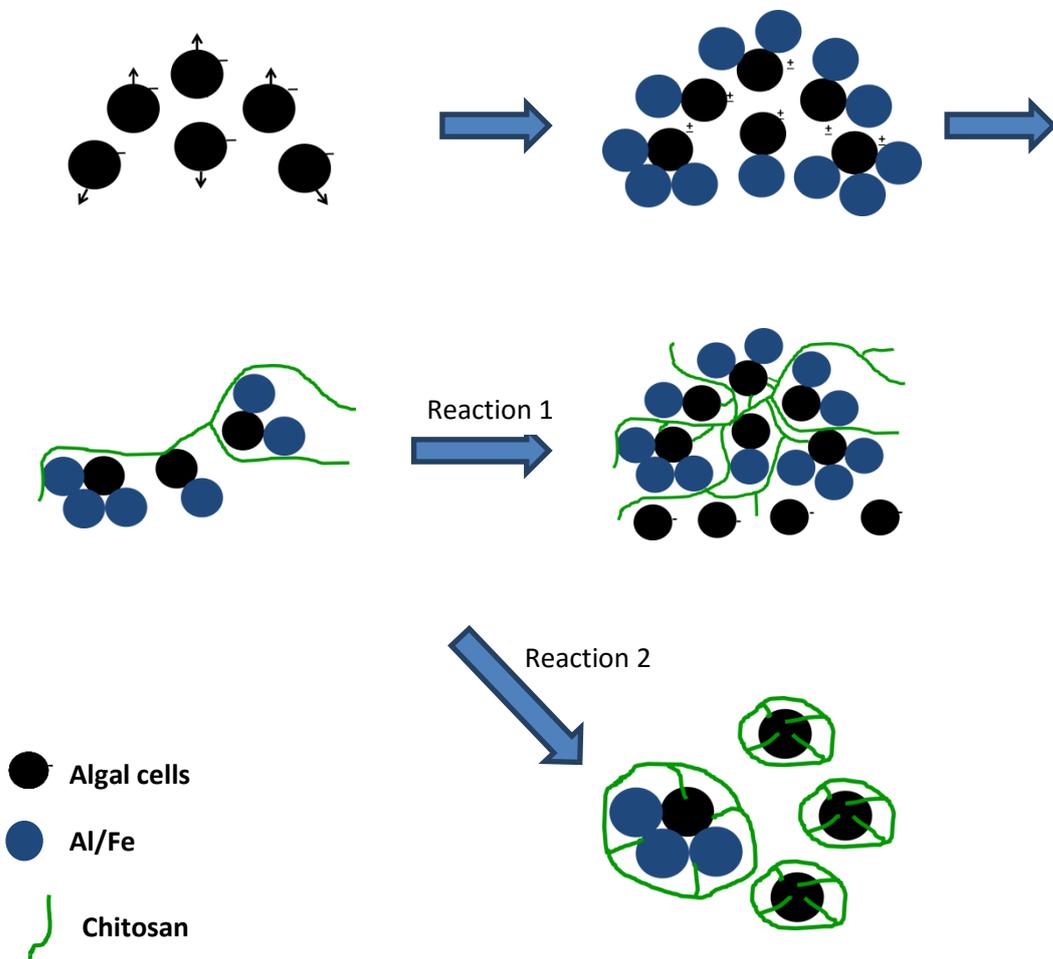
14 The alum addition during the rapid mixing lowered the charge of suspended microalgae, and allowed
 15 microflocs to form, after which a slight amount of chitosan added during the slow mixing facilitated
 16 further charge neutralization and enhanced bridging between microflocs.

17 Similar experiments were performed using a fixed dose of 5 ppm ferric chloride coagulant, and a
 18 varied dosage of chitosan as a flocculant aid. 97% microalgae removal efficiency (Figure 4F) was
 19 achieved for the ferric chloride: chitosan (5 ppm: 2.5 ppm) dose levels, with a sedimentation time of
 20 five minutes. Clarified water was filtered using 0.45 micron filter, and the residual iron concentration
 21 was found to be < $1\mu\text{g/L}$.

22 *3.4 Mechanism model for Dual Coagulation for HABs in seawater:*

23 The coagulation process took place after the effective elimination/lowering of the DLVO energy
 24 barrier, also referred to as *destabilization* [34]. An ionic concentration of sea water compressed the
 25 double layer around the microalgae particles. For low salinity waters, colloids can be destabilized by
 26 the addition of an indifferent electrolyte. Addition of indifferent electrolyte increases the ionic

1 strength of solution that has the effect of compressing the electrical double layer. Due to high
 2 salinity of the sea water, the counter ions are pushed closer to the surface the repulsion forces
 3 become easier to negate by van der Waals forces. Charge neutralization happened after the
 4 adsorption of a positively charged Al/Fe on the surface of microalgal particles. Charge neutralization
 5 produced an aggregation of microalgae particles to form bigger flocs. When chitosan was introduced
 6 during the coagulation stage, particle entrapment and bridging took place. These mechanisms
 7 contributed to a slight increase in microalgal removal efficiency (90%) when compared to the alum
 8 coagulation process, with a microalgae removal efficiency of 83% (Table 2). However, the flocs
 9 produced (Figure 5C) were similar to the flocs obtained for chitosan coagulation (Figure 5B), and
 10 required a longer (30 minutes) sedimentation time. During the dual coagulation, an overdose of
 11 chitosan led to charge reversal/re-stabilization, facilitated by reaction 2 of Figure 6. The process of
 12 charge reversal could be attributed to the effects of the rapid mixing, where a destabilized particle
 13 underwent a secondary adsorption of chitosan polymer by hindering the vacant sites of other nearby
 14 particles.



15

16 **Figure 6:** Mechanism model for dual coagulation. Reaction 1 Sweep Flocculation; Reaction 2 charge
 17 reversal/re-stabilization

18 In contrast, chitosan addition during flocculation stage (slow mixing) resulted in a macroflocs of size
 19 > 1cm (Figure 5 D), and the sedimentation time observed for this process was much shorter (five

1 minutes). This process was facilitated by a chitosan bridging of micro aggregates, and followed by a
2 sweep flocculation, as shown in reaction 1 of Figure 6. The orthokinetic/macroscale flocculation
3 induced the contact of particles through bulk fluid motion (gentle motion of fluid) and velocity
4 gradients in the liquid. The dual coagulation approach resulted in a lower residual of aluminium/iron.
5 Thus, the dual coagulation experiments were very efficient for microalgae laden seawater, as they
6 resulted in a shorter process time, with low doses of alum/iron coagulants and chitosan as a
7 flocculant aid. The C-F-S processes for seawater were governed by double layer compression,
8 charge neutralization, bridging and colloidal entrapment mechanisms.

9

10 **4 Conclusions**

11 Individual coagulations using alum, chitosan and FeCl_3 resulted in reduced levels of microalgae in
12 seawater feed for desalination. C-F-S experiments using FeCl_3 coagulant gave better process
13 performance (20 ppm FeCl_3 dose, raw water pH, 30 min sedimentation time and 98% microalgae
14 removal efficiency) when compared to alum and chitosan based individual coagulations. C-F-D
15 process demonstrated improved process performance with a reduced coagulant dosage
16 requirements and the process time (5 ppm FeCl_3 dose, raw water pH, 5 minutes flotation time).
17 Despite of its improved performance, energy requirements of the C-F-D process are proven to be
18 high, therefore alternate strategies were developed to improve the C-F-S process. The process time
19 of the coagulation process was significantly reduced by the addition of chitosan as a flocculant aid.
20 For dual coagulation using alum (10 ppm) as coagulant and chitosan (1ppm) as flocculant aid
21 improved microalgae removal efficiency to 98% at a reduced process time of 5 minutes, thus making
22 C-F-S process as attractive as C-F-D process. C-F-S processes for seawater were governed by double
23 layer compression, charge neutralization, bridging and colloidal entrapment mechanisms. Moreover,
24 the residual alum concentration in dual coagulation process using alum and chitosan was
25 significantly reduced when compared to alum based individual coagulation. Further studies will be
26 focused on economics of the above pre-treatment processes, and effects of microalgae on
27 membrane performance during sea water desalination.

28 **5 Acknowledgements:**

29 This article was made possible by the NPRP grant [NPRP9-159-2-087] from the Qatar National
30 Research Fund (a member of Qatar Foundation). The findings achieved herein are solely the
31 responsibility of the authors.

32 **6 References:**

- 33 [1] <http://www.unwater.org/publications/publications-detail/en/c/204294>.
- 34 [2] I. Bremere, M. Kennedy, A. Stikker, J. Schippers, How water scarcity will effect the growth in the
35 desalination market in the coming 25 years, *Desalination* 138(1–3) (2001) 7-15.
- 36 [3] S. Gorjian, B. Ghobadian, Solar desalination: A sustainable solution to water crisis in Iran,
37 *Renewable and Sustainable Energy Reviews* 48 (2015) 571-584.
- 38 [4] V.G. Gude, Desalination and sustainability – An appraisal and current perspective, *Water*
39 *Research* 89 (2016) 87-106.

- 1 [5] F. Macedonio, E. Drioli, A.A. Gusev, A. Bardow, R. Semiat, M. Kurihara, Efficient technologies for
2 worldwide clean water supply, *Chemical Engineering and Processing: Process Intensification* 51
3 (2012) 2-17.
- 4 [6] J.R. Ziolkowska, R. Reyes, Chapter 3.1.3 - Prospects for Desalination in the United States—
5 Experiences From California, Florida, and Texas, *Competition for Water Resources*, Elsevier 2017, pp.
6 298-316.
- 7 [7] B. Peñate, L. García-Rodríguez, Current trends and future prospects in the design of seawater
8 reverse osmosis desalination technology, *Desalination* 284 (2012) 1-8.
- 9 [8] G. Amy, N. Ghaffour, Z. Li, L. Francis, R.V. Linares, T. Missimer, S. Lattemann, Membrane-based
10 seawater desalination: Present and future prospects, *Desalination* 401 (2017) 16-21.
- 11 [9] D.A. Caron, M.-È. Garneau, E. Seubert, M.D.A. Howard, L. Darjany, A. Schnetzer, I. Cetinić, G.
12 Filteau, P. Lauri, B. Jones, S. Trussell, Harmful algae and their potential impacts on desalination
13 operations off southern California, *Water Research* 44(2) (2010) 385-416.
- 14 [10] J.K. Edzwald, J. Haarhoff, Seawater pretreatment for reverse osmosis: Chemistry, contaminants,
15 and coagulation, *Water Research* 45(17) (2011) 5428-5440.
- 16 [11] L. Henthorne, B. Boysen, State-of-the-art of reverse osmosis desalination pretreatment,
17 *Desalination* 356 (2015) 129-139.
- 18 [12] L.O. Villacorte, S.A.A. Tabatabai, D.M. Anderson, G.L. Amy, J.C. Schippers, M.D. Kennedy,
19 Seawater reverse osmosis desalination and (harmful) algal blooms, *Desalination* 360 (2015) 61-80.
- 20 [13] X. Zheng, D. Chen, Q. Wang, Z. Zhang, Seawater desalination in China: Retrospect and prospect,
21 *Chemical Engineering Journal* 242 (2014) 404-413.
- 22 [14] F.A. Abd El Aleem, K.A. Al-Sugair, M.I. Alahmad, Biofouling problems in membrane processes for
23 water desalination and reuse in Saudi Arabia, *International Biodeterioration & Biodegradation* 41(1)
24 (1998) 19-23.
- 25 [15] S. Huang, N. Voutchkov, S.C. Jiang, Investigation of environmental influences on membrane
26 biofouling in a Southern California desalination pilot plant, *Desalination* 319 (2013) 1-9.
- 27 [16] S.C. Leterme, C. Le Lan, D.A. Hemraj, A.V. Ellis, The impact of diatoms on the biofouling of
28 seawater reverse osmosis membranes in a model cross-flow system, *Desalination* 392 (2016) 8-13.
- 29 [17] Q. She, R. Wang, A.G. Fane, C.Y. Tang, Membrane fouling in osmotically driven membrane
30 processes: A review, *Journal of Membrane Science* 499 (2016) 201-233.
- 31 [18] H. Dieter, *Drinking Water Toxicology in Its Regulatory Framework A2 - Wilderer, Peter, Treatise*
32 *on Water Science*, Elsevier, Oxford, 2011, pp. 377-415.
- 33 [19] B.W. Ibelings, L.C. Backer, W.E.A. Kardinaal, I. Chorus, Current approaches to cyanotoxin risk
34 assessment and risk management around the globe, *Harmful Algae* 40 (2014) 63-74.
- 35 [20] S. Merel, D. Walker, R. Chicana, S. Snyder, E. Baurès, O. Thomas, State of knowledge and
36 concerns on cyanobacterial blooms and cyanotoxins, *Environment International* 59 (2013) 303-327.
- 37 [21] D. Pantelić, Z. Svirčev, J. Simeunović, M. Vidović, I. Trajković, Cyanotoxins: Characteristics,
38 production and degradation routes in drinking water treatment with reference to the situation in
39 Serbia, *Chemosphere* 91(4) (2013) 421-441.
- 40 [22] K. Loganathan, Ozone-based advanced oxidation processes for the removal of harmful algal
41 bloom (HAB) toxins: a review, *Desalination and Water Treatment*, 2016, pp. 1-7.
- 42 [23] S. Plantier, J.B. Castaing, N.E. Sabiri, A. Massé, P. Jaouen, M. Pontié, Performance of a sand filter
43 in removal of algal bloom for SWRO pre-treatment, *Desalination and Water Treatment* 51(7-9)
44 (2013) 1838-1846.
- 45 [24] M. Ferhat, S. Kadouche, N. Drouiche, K. Messaoudi, B. Messaoudi, H. Lounici, Competitive
46 adsorption of toxic metals on bentonite and use of chitosan as flocculent coagulant to speed up the
47 settling of generated clay suspensions, *Chemosphere* 165 (2016) 87-93.
- 48 [25] S. Kadouche, H. Lounici, K. Benaoumeur, N. Drouiche, M. Hadioui, P. Sharrock, Enhancement of
49 Sedimentation Velocity of Heavy Metals Loaded Hydroxyapatite Using Chitosan Extracted from
50 Shrimp Waste, *Journal of Polymers and the Environment* 20(3) (2012) 848-857.

- 1 [26] F. Renault, B. Sancey, P.M. Badot, G. Crini, Chitosan for coagulation/flocculation processes – An
2 eco-friendly approach, *European Polymer Journal* 45(5) (2009) 1337-1348.
- 3 [27] J.K. Edzwald, Dissolved air flotation and me, *Water Research* 44(7) (2010) 2077-2106.
- 4 [28] J. Haarhoff, J.K. Edzwald, Adapting dissolved air flotation for the clarification of seawater,
5 *Desalination* 311 (2013) 90-94.
- 6 [29] M.A.Z.M.R. Rozainy, M. Hasif, Syafalny, P. Pugeswary, A. Afifi, Combination of Chitosan and
7 Bentonite as Coagulant Agents in Dissolved Air Flotation, *APCBEE Procedia* 10 (2014) 229-234.
- 8 [30] Y. Shutova, B.L. Karna, A.C. Hambly, B. Lau, R.K. Henderson, P. Le-Clech, Enhancing organic
9 matter removal in desalination pretreatment systems by application of dissolved air flotation,
10 *Desalination* 383 (2016) 12-21.
- 11 [31] A.C. Twort, D.D. Ratnayaka, M.J. Brandt, Preface, *Water Supply* (Fifth Edition), Butterworth-
12 Heinemann, London, 2000, pp. ix-x.
- 13 [32] S.T. Cassini, S.A. Francisco, P.W.P. Antunes, R.N. Oss, R. Keller, Harvesting Microalgal Biomass
14 grown in Anaerobic Sewage Treatment Effluent by the Coagulation-Flocculation Method: Effect of
15 pH, *Brazilian Archives of Biology and Technology* 60 (2017).
- 16 [33] J.M. Li, Green algal over cyanobacterial dominance promoted with nitrogen and phosphorus
17 additions in a mesocosm study at Lake Taihu, China, *Environ Sci Pollut Res*, 2015, pp. 5041–5049.
- 18 [34] J.M. Ebeling, P.L. Sibrell, S.R. Ogden, S.T. Summerfelt, Evaluation of chemical coagulation–
19 flocculation aids for the removal of suspended solids and phosphorus from intensive recirculating
20 aquaculture effluent discharge, *Aquacultural Engineering* 29(1–2) (2003) 23-42